

NEW YORK CONTRACTOR'S EXPERIENCE WITH PERFORMANCE TESTING

2021 NORTH EAST ASPHALT USER PRODUCER GROUP

VIRTUAL MEETING







HISTORY OF MIX DESIGN

Barber Asphalt Paving Company

• Asphalt cement 12 to 15% / Sand 70 to 83% / Pulverized carbonite of lime 5 to 15%

Clifford Richardson, New York Testing Company

- Surface sand mix: 100% passing No. 10, 15% passing No. 200, 9 to 14% asphalt
- •Asphaltic concrete for lower layers, VMA terminology used, 2.2% more VMA than current day mixes or ~0.9% higher binder 905 content

• Hubbard Field Method (Charles Hubbard and Frederick Field) •Sand asphalt design

920s •30 blow, 6" diameter with compression test (performance) asphaltic concrete design (Modified HF Method) Stability

• Francis Hveem (Caltrans)

- Surface area factors used to determine binder content; Hveem stabilometer and cohesionmeter used
- Air voids not used initially, mixes generally drier relative to others, fatigue cracking an issue **Stability + Durability**

• Bruce Marshall, Mississippi Highway Department

943

1993

927

890

• Refined Hubbard Field method, standard compaction energy with drop hammer •Initially, only used air voids and VFA, VMA added in 1962; stability and flow utilized

Stability + Durability

- Superpave
- Level 1 (volumetric)
- Level 2 and 3 (performance based, but never implemented)

В





Performance Based Specification

Introduction

The Northeast Asphalt User Producer Group's (NEAUPG) Asphalt Mix Committee is looking closely as a region at Performance Based Specifications (PBS). The Committee would like to provide state agencies in the Northeast with information on laboratory tests which will closely predict asphalt pavement performance in the field over a typical design life. We expect that this process will require multiple tests based on differing criteria and performance characteristics. The eventual objective is to allow states the opportunity to maintain specifications that meet their needs while allowing producers/contractors the means to deviate from those specifications if the require tests are run and criteria are met on mixes in the laboratory

We are reaching out to research centers, State Materials Engineers, and stake laboratory tests that may be used to predict in place performance and if ther effect. This includes the actual test, test protocols, and possible standards.

We appreciate your participation in this Survey. All results will be kept confi report. You will be sent a full copy of Survey results when finalized.

Thank you for your time in this matter.

Respectfully yours,

NEAUPG Mix Committee

Co-chairs: Edmund Naras – Pavement Management Engineer, MassDOT Bruce Barkevich – Vice President, New York Construction Mate **Optimized Mix Design for Performance**

NORTHEAST ASPHALT USER PRODUCER GROUP (NEAUPG)

ANNUAL MEETING BURLINGTON, VERMONT OCTOBER 2015



SHANE BUCHANAN OLDCASTLE MATERIALS





Development of a Semicircular Bend (SCB) Test Method for Performance Testing of Nebraska Asphalt Mixtures

Gabriel Nsengiyumva

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Yong-Rak Kim, Ph.D. Associate Professor **Department of Civil Engineering** University of Nebraska-Lincoln

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2015

Nebraska Transportation Center 262 WHIT 2200 Vine Street Lincoln, NE 68583-0851 (402) 47 2-197 5

This report was funded in part through grant(s) from the Federal Hi The views and opinions of the authors [or agency] expressed h

Technology Program is an integrated, national effort to improve the long-term performance and cost effectiveness of asphalt pavements. Manag Federal Highway Ar through partnerships with state

academia the program's primary goals are to reduce congestion, improve safety, and foster technology innovation

The program was established to naterials selection, mixture design, testing, construction

2 IS Rund THE LC TRAPH MUD. Faderal Highway Administration

and quality control.

Office of Asset Management. Pavements, and Construction FHWA-HIF-14-015 September 2014

TechBrief

Introduction

At the conclusion of the Strategic Highway Research Program (SHRP) over 20 years ago, it was envisioned that the new asphalt mix design system would have three levels based on the design traffic for the pavement. Level I was envisioned to be for low traffic pavements and the mix design requirements would be primarily based on traditional volumetric properties. Level II would be used for the majority of projects that carry moderate traffic levels and would include volumetric requirements plus a limited set of mixture performance tests. Level III would be for high traffic pavements also start with a volumetric based mix design followed by an expanded set of advanced performance tests. However, the "performance tests" were never implemented, except for a few special projects, primarily because

The Need for Asphalt Mixture Cracking

Tests and the Steps Toward

Implementation

This Technical Brief covers the motivations for pursuing

asphalt mixture cracking tests, provides an overview of

necessary steps toward implementation, and identifies

the different cracking test methods, describes the

gaps where further research is needed.

the tests were not considered practical for routine use for the thousands of mix designs used each year in the United States.

Early in the implementation of Superpave mix design, more focus was given to addressing rutting. Mix designs for moderate and high traffic pavements were designed to improve rutting resistance by following more restrictive aggregate requirements and the binder grade bumping guidelines. Many states also added rutting test requirements to mix designs for moderate and high traffic projects. As the early projects built under the Superpave system have matured, most highway agencies have recognized that rutting problems have been virtually eliminated.

NCHRP **REPORT 704**

NATIONAL

HIGHWAY

RESEARCH

PROGRAM

COOPERATIVE

TRAN

A Performance-Related Specification for Hot-Mixed Asphalt

TRANSPORTATION RESEARCH BOARD OF THE NATIONAL ACADEMIES



December 28, 2015

CIRCULAR LETTER 2015-19

ILLINOIS FLEXIBILITY INDEX TEST - PILOT PROJECTS

COUNTY ENGINEERS / SUPERINTENDENTS OF HIGHWAYS MUNICIPAL ENGINEERS / DIRECTORS OF PUBLIC WORKS / MAYORS METROPOLITAN PLANNING ORGANIZATIONS - DIRECTORS TOWNSHIP HIGHWAY COMMISSIONERS CONSULTING ENGINEERS

The department has been developing a new hot-mix asphalt (HMA) performance test for durability through research at the Illinois Center for Transportation. This new performance test is known as the Illinois Flexibility Index Test (I-FIT). The objective of the I-FIT test is to ensure HMA mixtures have the necessary flexibility to resist premature cracking.

The department is preparing to implement the newly developed test on a pool of pilot projects during the 2016 construction season. The department is asking for local public agency volunteers interested in participating with the pilot program. The department will evaluate these pilot projects through our experimental feature process.

The Illinois Flexibility Index Test is performed on pucks prepared from either gyratory compacted HMA or six-inch cores taken from in-place pavement.

Testing and Analysis of LWT and SCB **Properties of Asphaltic Concrete Mixtures**

Samuel Cooper III

Louisiana Transportation Conference February 18 - 20, 2013 Baton Rouge, Louisiana





| A. | Mix | Virgin | 10% RAP "S" | 15% RAP "S" | 20% RAP "S" | 20% RAP "V" |
|----|--------|-------------|----------------|----------------|----------------|----------------|
| | 19.0mm | | - | ÷ | 6.0 | 4.1 |
| | 12.5mm | | - | 4.6 | 6.0 | - |
| | 9.5mm | 3.1 | 1.2 | - | 3.5 | 2.5 |









3348 Route 208, Campbell Hall, NY 10916 Phone: 845-496-1600 Fax: 845-496-1398 42 Day Farm Road, West Stockbridge, MA 01266 Phone/Fax: 413-232-8566

Hamburg Wheel-Track Testing of Compacted HMA Test Method AASHTO T 324

| Client: | Barree Stone Products | Project | QC- Hamburg Testing Albion, NY |
|---------------|-------------------------|-----------------|-----------------------------------|
| Material: | 12.5 mm < 0.3m, 20% RAP | Project Number: | 160954 |
| Source: | Barrie | Lab Number: | 16-1488 |
| Date Sampled: | 11/1/2018 | Sampled By: | Client |
| Date Tested: | 11/14/2016 | Tested By: | John Brinsfield |



















































| | 4 | 8 | C | D | E | F G | 8 | 1 | 4 | 0 | 4 | M | R | D | | 9 | | 5 | T | Ų | ¥ | W | - |
|----|---------------------|---------------------|----------------------|------------------|------------------|-------------|----------------|---------|---------|---------|---|----|-----|--------------------------|------------|-------------|-----------|-----------|-------------------------------|---|-----------------|-----------|---------|
| ī | Directions: | Fill in gellow a | ells and use the | solver on blu | e cells | | | | | | | | | | | | _ | - | | | | | |
| ź | Project | Barre Stone Produc | ts. 12.5mm c 03. PG6 | 45-22, 20% RAP | | | | | | | | | | | | | | | | | | | |
| ŝ | Sample D | 072816-316-12-2 | L | | | | | | | | | | | | | | | | | | | | |
| 4 | Target AV/% | 55 | | | | | | | | | | _ | | | - | | _ | | | | | | |
| 5 | Air Voids | 2.35 | | | | | | | | | | | | | | | | | | | | | |
| 5 | Dimensional | Netch (15mm) | Thickness (SOmm) | Ligament Length | | | | | | | | | | Y4.01 | UNISIN/244 | 19057AU800v | 1.1.1.111 | 02134910 | 100000 ⁴ 2.5183425 | 28215080000004 + LL 415 | 10100470790 | 1, 100000 | |
| ī | Measurement 1 | 15.83 | 52.04 | 56.1 | | | | | | | | - | | | | 1.34037688 | 601E50000 | 11 + 5000 | 40034566254 5108000 | 004 + 5 402278161091000 | 00000 | | |
| 8 | Measurement 2 | 15.71 | 52.29 | 55.91 | | | | | | | | | | | 1 | | | 194 | 9181111195-40006808 | 800 | | | |
| 2 | Measurement 3 | | 52.1 | | | | | | | | | | | | 1 | | | | | | | | |
| 0 | Average | 15.77 | 52.14333333 | 56.005 | | | | | | | | | | | 1 | | | | | | | | |
| 1 | | | | | | | and the second | | | | | | | | | | | | | | | | |
| 2 | | _ | Raw Data | _ | | - | Processed | Data | | | | | | | | | | | | | | | |
| 3 | X-exis (# of Lines) | Y-Axis (# of Lines) | Conversion to lbs | Conversion to kn | Conversion to mm | Stroke (mm) | Load (kN) | P | P | | | - | | | | 1 | | | | | | | |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13.4002 | -42,681 | 0.07061 | | 1 | | | | 1 | | | | _ | | | |
| 8 | 1 | 10 | 250 | 11120354 | 0.127 | 0.127 | 1 1120554 | 8.5092 | -34.524 | 0.21185 | | | | | | | 1 | | | | | | |
| 1 | 2 | 20 | 500 | 2.2241108 | 0.254 | 0.254 | 2.1241108 | 4.58669 | -27.415 | 0.54955 | | I | - | | | | N | | | | | | |
| 8 | 5 | 29.5 | 737.5 | 3.28056343 | 0.381 | 0.381 | 3.28056343 | 1.9051 | -21.268 | 0.46959 | | | | | | | | - | Langener. | Bitternet | | | |
| 9 | 4 | 37 | 925 | 4,11450498 | 0.508 | 0,508 | 411460498 | -0.8525 | -16 | 0.56492 | | 0 | 1 | | | | | | 1.000 | mana | | | |
| 0 | 3 | 43 | 1075 | 4.78183822 | 0.635 | 0.635 | 4,78185822 | -2.5929 | -11.555 | 0.63907 | | | 0 | 1 | | 2 | | 5 | | á 3 | | | |
| 1 | 5 | 47.5 | 1187.5 | 5.28226315 | 0.782 | 0.762 | 5 28226315 | -3.8131 | -7.7959 | 0.6885 | | | | | | | _ | | | La constante da | | | |
| 1 | 1 | 50 | 1250 | 5.560277 | 0.889 | 0.889 | 5.560177 | -4.6008 | -47118 | 0.70969 | | | | | | - | | | Raw Coefficients | Integral Coefficients | | | |
| 3 | 1 | 50.5 | 1262.5 | 5,61387977 | 1.016 | 1.016 | 3.81387977 | +5.0547 | -2.2142 | 0.70262 | | | | Start | Finish | Infection | Max Lord | . 6 | -0.018050424 | -0.002578632 | W | F(Joules) | 9.420 |
| 4 | | 49 | 1225 | 5,44907145 | 1.143 | 1.143 | 5.44907145 | -5,1853 | -0.2582 | 0.66579 | | L. | oed | 5.402278161 | 6.2275 | 5,48359 | 5.61588 | 5 | 0.567590215 | 0.061231702 | | | |
| 5 | 10 | 43 | 1125 | 5.0042493 | 1.27 | 1.27 | 5.0042495 | -5.1147 | 1.27777 | 0.60023 | | 0 | Nap | 0 | 1015 | 1.16075 | 1,018 | | -2.953542928 | -0.586708586 | | | |
| 0 | 11 | 40 | 1000 | 4.4482216 | 1.597 | 1.397 | 4,4482216 | -4.8777 | 2.39192 | 0.51902 | | | | | | | | | 11.4296916 | 2.857422901 | | | |
| 17 | 12 | 33.5 | 837.5 | 3.72538559 | 1.524 | 1.524 | 5.72558559 | -4.5218 | 3.15905 | 0.43429 | | | | | | | | 2 | -21.34037467 | -7.113458222 | | | |
| 8 | 13 | 28 | 700 | 3.11375512 | 1.651 | 1.651 | 3.11373512 | -4.0878 | 3.63059 | 0.36014 | | | | | | | | 1 | 13.4001656 | 6.700082801 | | | |
| 9 | 14 | 23 | 575 | 2.55772742 | 1.778 | 1.778 | 2 55772742 | -3.6101 | 3.85459 | 0.19659 | | | | | | | | 0 | 5.402278161 | 5.402278161 | | | |
| 0 | 15 | 19 | 475 | 2 11290526 | 1.905 | 1.905 | 2.11290526 | -5.1175 | 3.87571 | 024715 | | | | | | | | | and the second second | | | | |
| 1 | 16 | 16 | 400 | 1.77928864 | 2,032 | 2.052 | 1,77928864 | -2.6525 | 3.75525 | 0.21185 | | | 100 | Area(ile) | 0.00292 | | | Note | Adjust the trend ine | to go from the peak loa | d to final load | and paste | the com |
| 1 | 17 | 14 | 350 | 1.55687756 | 2.159 | 2.159 | 1.55687756 | +2.1738 | 3.47106 | 0.1836 | | | | Gf (louies/m2) | 3225.75 | | | | | | | | |
| 3 | 13 | 12 | 300 | 1.33446648 | 2.286 | 2.286 | 1.33446648 | -1.7547 | 3,11771 | 0.13535 | | | | Secont Stillness | 5.52744 | | | | | | TITGE | under . | |
| 4 | 19 | 10 | 250 | 1.1120554 | 2.413 | 7.413 | 1.1120554 | -1.5844 | 2.70655 | 0.15417 | | | | Flexibility Index | 6.21847 | | | | | THEFT | 1766 | SY | |
| 5 | 20 | 9 | 225 | 1.00084986 | 1.54 | 2.54 | 1.00084986 | -1.0685 | 2.26468 | 0.12005 | | | | alerna in | | | | | | 136 | | 812 | S FE |
| 8 | 23 | 8 | 200 | 0.88964452 | 2.667 | 2.667 | 0.88964452 | -0.8094 | 1.81713 | 0.10592 | | | | -5.187566426 | 3225.75 | 5.21847 | | | | ĨĨ | | E | 2 |
| 17 | 12 | 7 | 175 | 0,77843878 | 2,794 | 2.794 | 0.77843878 | -0.6063 | 1.38469 | 0.09392 | | | | | | | | | | C.N. | | | A7 |
| 8 | 23 | 63 | 157.5 | 0.700594902 | 2.921 | 2.921 | 0.700594902 | -0.4563 | 0,98497 | 0.08544 | | | | | | | | | | HE A | | A | |
| 9 | 24 | 5.8 | 145 | 0,544992132 | 3,048 | 3.048 | 0.644992152 | -0.3542 | 0.6522 | 0.07658 | | | | | | | | | | | · occipi | | m |
| 0 | 23 | 5.5 | 132.5 | 0.589389362 | 3.175 | 3.175 | 0.589389362 | -0.2933 | 0.35725 | 0.07132 | | | | | | | | | | A A A A A A A A A A A A A A A A A A A | RSITE | THURSDAY | |
| i | 34 | 2.8 | .120 | 0.483756503 | 8 503 | 8 8/12 | 0.555786502 | -0.1657 | 0.10758 | 19130.0 | | | | | | | | | | | | | |





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2019 SPECIAL NOTE ASPHALT MIXTURE PERFORMANCE TESTING

NYSDOT & INDUSTRY V1.00







SPECIAL NOTE ASPHALT MIXTURE PERFORMANCE TESTING

This Special Note requires the asphalt producer to collect asphalt mixture during the production for this project. The Producer will perform the following tasks and the cost of producing, shipping, and testing these specimens at an AMRL approved laboratory capable of performing these tests and at the Producer laboratory will be included in the bid price of the asphalt mixture. The Producer and RME will agree on the production day to implement the requirements of this note.

Task 1. Collection of Asphalt Mixture.

The Producer shall collect mixture for testing as follows on a two sublot day production:

Sublot 1 – Testing Lab and Producer Lab

Sublot 2 - Producer Lab only

- a) The producer shall supply sufficient mixture to the AMRL approved laboratory so that the required specimens can be fabricated and tested as listed in Task 2.
- b) The Producer shall collect sufficient mixture to fabricate specimens in their lab and tested as listed in Task 3.

The mixture shall be collected after the first 300 tons. If the production is such that it yields only one sublot, then it will be divided into two sublot for the day.







Task 2. Number of Specimens (Testing Lab).

The testing laboratory will make the following number of specimens for performance testing:

- a. Overlay Tester 5 specimens
- b. Asphalt Pavement Analyzer (APA) or Hamburg Wheel Tracker 6 specimens
- c. Semi-circular Bend (SCB) 4 specimens
- d. Ideal-CT 3 specimens
- e. High Temperature Indirect Tension 3 specimens
- f. Gradation
- g. Asphalt content using chemical extraction.

Task 3. Number of Specimens (Producer Lab).

The producer will make the following number of specimens for performance testing:

- a. Semi-circular Bend (SCB) 4 specimens
- b. Ideal-CT 3 specimens
- c. High Temperature Indirect Tension 3 specimens

Task 4.

<u>Test Results.</u> The Producer will submit both the testing lab and Produce lab results to the Materials Bureau once the tests are completed. In addition, the Producer shall submit the volumetric results of the mixture during the production for the day selected. The QAF will be a 1.0.

Page 1 of 1







| Date when the Quick <u>NOTE</u> : 1. The user and the include all the needer form is sent to the C than the one used to to reflect the Price A actually performed. | Quote form is sent Contractor understa of Price Adjustments ontractor). If the pr calculate this Quick djustments for the M | to the Contractor: April and that the Project's Total Cost t for the month indicated (the mon oject (or part of the project) is exe Quote, then the Project's Total C Ionth in which the project (or par | / <u>3</u> / 20 <u>19</u> o be shown below will oth when the Quick Quote ecuted in a different month cost will change accordingly rt of the project) was |
|---|--|---|---|
| NOTE: 1. The user and the include all the needed form is sent to the C than the one used to to reflect the Price A actually performed. | Contractor understa of Price Adjustments ontractor). If the pr calculate this Quick adjustments for the M | nd that the Project's Total Cost t for the month indicated (the mon oject (or part of the project) is exe Quote, then the Project's Total C Ionth in which the project (or par | o be shown below will oth when the Quick Quote ecuted in a different month cost will change accordingly rt of the project) was |
| 2. The Contractor u <u>Adjustment) exceed</u> Contractor any time | nderstands that <u>at n</u> <u>the contract price</u> . during the quick qu | o time may a quick quote unit pri Materials cost, hauling expenses, ote process. | ice (without the Price etc., can be lowered by the |
| Agency/User: | NYSDOT Monro | be County West Residency | |
| Project Name: | NY 19 FOB Pav | ng | Project # 401982 |
| | NV 10 from NV | 104 to NY 18 | |
| Project Location: | INT IS HOM INT | | AND STORE STORES |
| Project Location: County: | Monroe | City: T/o Clarkson/Hamlin | Zip Code: 14420 |











LS

BR 257



| Producer | | 1111 - C |
|-------------------|----------|----------------|
| BAR | Plant ID | INC. Region |
| Barre 6 Ton Batch | H0306 | 4 |

| Туре | PG Binder | Additive | Coding | Site Manager # |
|------|----------------------------------|--|--|--|
| HMA | PG 64S-22 | | 9F32HB | H030618154 |
| HMA | PG 64V-22 | | 9F32HC | 4030618154 |
| WMA | PG 64S-22 | EVO | 9F32WB | 14030618155 |
| WMA | PG 64V-22 | EVO | 9F32WC | HO306 18 155 |
| | | | | - |
| | | | | |
| | Type HMA HMA WMA WMA | Type PG Binder HMA PG 64S-22 HMA PG 64V-22 WMA PG 64S-22 WMA PG 64S-22 | TypePG BinderAdditiveHMAPG 64S-22HMAPG 64V-22WMAPG 64S-22EVOWMAPG 64V-22EVOWMAPG 64V-22EVO | TypePG BinderAdditiveCodingHMAPG 64S-229F32HBHMAPG 64V-229F32HCWMAPG 64S-22EVO9F32WBWMAPG 64V-22EVO9F32WCWMAPG 64V-22EVO9F32WC |

| A mark | | Source | DI 3.0/ | Dland | Blend Lim | its to Maint | ain C.A.P.'s |
|--------|--------------------------|--------|---------|---------------|---------------|--------------|----------------|
| Aggi | regates | Number | Blend % | Blend | C.A.A. | F.A.A. | Flat/Elong |
| | No. 3A Stone | | | | | 115 5 1 | |
| | No.2 Stone | | | | | | |
| | No. 1 Stone | | | 1 Fric. Blend | | | 0 |
| Coarse | No. 1 Stone NC Stone | | | | * | 1. 1. 1. 1. | |
| | No. 1A Stone | 4-18R | 47 | IA Fric.Blend | 49 | 10000 | 0 |
| | No. 1A Stone NC Stone | | | 100/0 | | Burger | 17.10 |
| | No. 1B Stone | 4-18R | | Fines Blend | all's all | 50.2 | C. Markey |
| Fine | Man. Sand | | 33 | 2/1 | Mr. n. H | | 1 th to de- |
| A LINE | Natural Sand | 4-49F | | 2/1 | 7 | 38.4 | and the second |
| | Mineral Filler | | | | and the state | ALM CAR | |
| | RAP | Barre | 20 | | 52 | 46.0 | 1.0 |

| Sie | ve Size | 0.075mm | 0.150mm | 0.300mm | 0.600mm | 1.18mm | 2.36mm | 4.75mm | 9.5mm | 12.5mm | 19.0mm | 25.0mm | 37.5mm | 50.0mm | % Binder |
|---------------|-------------------|-------------|---------|---------|---------|---------|--------|---------|----------|----------|-----------|------------|--------------------------|-----------|----------|
| | General Limits | 2 - 10 | | | | | 32-67 | ≤90 | 90 - 100 | 97 -100 | 100 | | Design the second second | | 5.8 Min. |
| % Passing | JMF Range | 0-7 | 0-9 | 4 - 14 | 11-21 | 17 - 27 | 29-39 | 63 - 73 | 95 - 100 | 95 - 100 | 100 | Same Ad | | | YAM |
| - | Target Value | 2 | 4 | 9 | 16 | 22 | 34 | 68 | 100 | 100 | 100 | The second | | | 6.2 |
| | | | | | N 1 | 10 | | | | | | | | Virgin AC | 4.9 |
| | Pre | epared By : | | AN Greg | Rose ,* | AC | Date : | Aug- | -2018 | | Revisions | % Binder | | | |
| | | | 11 | 1111 | 11 | | | | | | 09/18 | 6.3 | | | |
| ccepted for ' | Verification/Proc | luction By: | J. | 1 Ral | All | - | Date: | 08/1 | 7/2018 | | / | | | | |





















| Mix Gmm: | 2.510 | |
|-----------------------|------------|------------------------|
| Sample Height (mm): | 62 | 62mm for Ideal-CT |
| Target Air Voids (%): | 7.0 | 7.0% for Ideal-CT |
| Trial Weights* : | 2500 1.023 |] |
| Rounded Weights: | 2500 | Ideal-CT Sample Weight |
| Sample Height (mm): | 95 | 95mm for HT-IDT |
| Target Air Voids (%): | 7.0 | 7.0% for HT-IDT |
| Trial Weights* : | 3842 1.02 | |
| Rounded Weights: | 3840 | HT-IDT Sample Weight |
| Sample Height (mm): | 160 | 160mm for SCB |
| Target Air Voids (%): | 8.5 | 8.5% for SCB |
| Trial Weights* : | 6429 1.01 | 1 |
| Rounded Weights: | 6430 | SCB Sample Weight |
| Input | | |
| Correction Factor | | |







NN/















| Plant Production | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
|------------------|-------|--------|-------------|--------|-----------|--------|
| Voids | % | 3.16 | 2.5 - 4.5 | 4.53 | - | 3.69 |
| VMA | % | 16.4 | > 15.0 | 16.73 | - | 16.03 |
| VFB | % | 76.5 | 65.0 - 80.0 | 72.92 | - | 76.99 |
| AC Content | % | 6.3 | 6.1 - 6.5 | 6.5 | 6.3 | 6.3 |
| | | | | | | |
| Plant Gradation | Units | Target | Range | Lot 4A | Rutgers * | Lot 4B |
| 1/2" | % | 100 | 100 | 100 | 100 | 100 |
| 3/8" | % | 100 | 95 - 100 | 99.7 | 98.5 | 99.7 |
| #4 | % | 68 | 63 - 73 | 69.9 | 72.7 | 70.9 |
| #8 | % | 34 | 29 - 39 | 31.3 | 35.3 | 33.6 |
| #16 | % | 22 | 17 - 27 | 19.6 | 22.3 | 21.5 |
| #30 | % | 16 | 11 - 21 | 13.1 | 15.7 | 14.5 |
| #50 | % | 9 | 4 - 14 | 7.8 | 10.9 | 8.3 |
| #100 | % | 4 | 0 - 9 | 4.3 | 7.7 | 4.2 |
| #200 | % | 2 | 0 - 7 | 2.4 | 5.7 | 2.1 |







APA, HAMBURG & OVERLAY

| APA Rutting @ 8,000 Cycles @ 64°C | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
|---|--------|--------|-----------|--------|---------|--------|
| Rut Depth | mm | | 4 - 7 | - | 4.38 | - |
| | | | | | | |
| Hamburg Rutting at 20,000 Cycles @ 50°C | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
| Rut Depth | mm | < 12.5 | n/a | - | 10.45 | - |
| | | | | | | |
| Overlay Test for Crack Resistance @ 25°C | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
| # of Cycles to Failure | Cycles | | 100 - 700 | - | 1171 | - |



This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.



long-term pavement performance (LTPP) database intermedi-

ate temperatures. The test method describes the determination

of the cracking tolerance index, CT_{Index}, and other parameters

determined from the load-displacement curve. These param-

eters can be used to evaluate the resistance of asphalt mixtures

Standard Test Method for **Determination of Cracking Tolerance Index of Asphalt** Mixture Using the Indirect Tensile Cracking Test at Intermediate Temperature¹

This standard is issued under the fixed designation D8225; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (e) indicates an editorial change since the last revision or reapproval.

1. Scope

to cracking.

2. Referenced Documents

2.1 ASTM Standards:² 1.1 This test method covers the procedures for preparing,

D8 Terminology Relating to Materials for Roads and Pavetesting, and measuring asphalt mixture cracking resistance using cylindrical laboratory-prepared asphalt mix samples or ments pavement cores. Testing temperatures are selected from the

D3203/D3203M Test Method for Percent Air Voids in Compacted Asphalt Mixtures

D3666 Specification for Minimum Requirements for Agencies Testing and Inspecting Road and Paving Materials D6373 Specification for Performance Graded Asphalt Binder

D6925 Test Method for Preparation and Determination of the Relative Density of Asphalt Mix Specimens by Means

Standard Method of Test for

Determining the Fracture Potential of Asphalt Mixtures Using the Flexibility Index Test (FIT)

AASHTO Designation: TP 124-18¹

Technical Section: 2d, Bituminous Materials

Release: Group 3 (August)





| CEDC | | |
|---|-----------------------|---------------|
| GERS ter for Advanced Infrastructure Transportation | s Asphalt Analysis To | ol Pack |
| | | |
| | | |
| Intermediate Temp SCB | HT-IDT | Cold Temp SCB |
| Ideal-CT | DCT | APA |
| | | |
| | | |











| | ASTM D6931 - 1 | 7 | | | | |
|---|--|------------------------------|-------------------------|--|--|--|
| Standard Test Method for Indirect Tensile (IDT) Strength of Asphalt Mixtures | | | | | | |
| | | | | | | |
| Project Name: | NYSDOT R4 - AMP Testing | Institution: | Barre Stone | | | |
| Project Name: Mix Type: | NYSDOT R4 - AMP Testing 9.5 F3, PG64S-22, 20% RAP | Institution: Date Tested: | Barre Stone 05/30/19 | | | |

| Specimen ID | L4A A | L4A C | L4A K | Average | Standard Deviation | COV (%) |
|--------------------|-------|-------|-------|---------|-----------------------|---------|
| Air Voids (%) | 7.0 | 7.0 | 7.1 | 7.0 | 0.0 | 0.7 |
| Thickness (mm) | 94.7 | 94.7 | 95.0 | 94.8 | 0.1 | 0.1 |
| Diameter (mm) | 150.0 | 150.0 | 150.0 | 150.0 | 0.0 | 0.0 |
| Peak Load (N) | 4884 | 5258 | 6472 | 5538 | 677.9 | 12.2 |
| IDT Stregth (kPa) | 219 | 236 | 289 | 248.0 | 30.0 | 12.1 |
| IDT Strength (psi) | 31.8 | 34.2 | 42.0 | 36.0 | 4.4 | 12.1 |











HIGH TEMPERATURE IDT

| High Temperature Indirect Tensile Strength (HT-IDT) @ 42°C | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
|---|---------------------------|----------------------|---------------------------------------|-----------------------|---|-----------------------|
| Voids | % | 7.0 | 6.5 - 7.5 | 7.0 | 7.0 | 6.9 |
| Thickness | mm | 95.0 | 94.0 - 96.0 | 94.8 | 95.5 | 95.0 |
| Diameter | mm | 150.0 | | 150.0 | 149.9 | 150.0 |
| Peak Load | Ν | | | 5538.0 | 5146.7 | 5563.2 |
| HT-IDT | kPa | | 158 - 324 | 248.0 | 228.9 | 248.7 |
| HT-IDT | PSI | | 23 - 47 | 36.0 | 33.2 | 36.1 |
| | | | | | | |
| High Temperature Indirect Tensile Strength (HT-IDT) @ 44°C | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
| Voids | | | | | | |
| | % | 7.0 | 6.5 - 7.5 | - | 7.3 | - |
| Thickness | % mm | 7.0 95.0 | 6.5 - 7.5 94.0 - 96.0 | - | 7.3 95.1 | - |
| Thickness Diameter | mm mm | 7.0 95.0 150.0 | 6.5 - 7.5 94.0 - 96.0 | - - - | 7.3 95.1 150.0 | - - - |
| Thickness Diameter Peak Load | % mm mm N | 7.0 95.0 150.0 | 6.5 - 7.5 94.0 - 96.0 | - - - - | 7.3 95.1 150.0 5320.0 | - - - - |
| Thickness Diameter Peak Load HT-IDT | % mm mm N kPa | 7.0 95.0 150.0 | 6.5 - 7.5 94.0 - 96.0 158 - 324 | - - - - - | 7.3 95.1 150.0 5320.0 237.2 | - - - - - |







| Specimen Information | | | | | |
|----------------------|------|--|--|--|--|
| ID | 1 | | | | |
| Thickness (mm) | 61.9 | | | | |
| Diameter (mm) | 150 | | | | |

| Analysis Results | | |
|--------------------------|---------|--|
| P100 (kN) | 21.093 | |
| L100 (mm) | 3.607 | |
| P85 (kN) | 17.788 | |
| P65 (kN) | 13.598 | |
| L85 (mm) | 4.745 | |
| L65 (mm) | 5.410 | |
| L75 (mm) | 5.077 | |
| m75 | 6.297 | |
| Work of Fracture (kN.mm) | 104.987 | |
| Fracture Energy (kN/mm) | 0.011 | |
| СТ | 60.69 | |



| | Raw Data | | | Data A | nalysis | |
|-------|--------------------|-------|--------|----------------|--------------|----------------|
| Load | Displacement (in) | Time | Load | Post-Peak Load | Displacement | Work Increment |
| (lbf) | Displacement (m.) | (sec) | (kN) | (kN) | (mm) | (kN.mm) |
| | 13 0 | 0.000 | 0.058 | 0.000 | 0.000 | 0.000 |
| | 13 0 | 0.133 | 0.058 | 0.000 | 0.000 | 0.000 |
| | 13 0 | 0.266 | 0.058 | 0.000 | 0.000 | 0.000 |
| | 13 0 | 0.399 | 0.058 | 0.000 | 0.000 | 0.000 |
| | 13 0 | 0.532 | 0.058 | 0.000 | 0.000 | 0.000 |
| | 48 0.0011 | 0.665 | 0.214 | 0.000 | 0.028 | 0.004 |
| | 64 0.0015 | 0.798 | 0.285 | 0.000 | 0.038 | 0.003 |
| | 187 0.005 | 0.931 | 0.832 | 0.000 | 0.127 | 0.050 |
| | 348 0.0076 | 1.064 | 1.548 | 0.000 | 0.193 | 0.079 |
| | 542 0.0109 | 1.197 | 2.411 | 0.000 | 0.277 | 0.166 |
| | 767 0.014 | 1.330 | 3.412 | 0.000 | 0.356 | 0.229 |
| 1 | 033 0.0179 | 1.463 | 4.595 | 0.000 | 0.455 | 0.397 |
| 1 | 321 0.0222 | 1.596 | 5.876 | 0.000 | 0.564 | 0.572 |
| 1 | 612 0.0263 | 1.729 | 7.171 | 0.000 | 0.668 | 0.679 |
| 1 | 898 0.0309 | 1.862 | 8.443 | 0.000 | 0.785 | 0.912 |
| 2 | 176 0.0358 | 1.995 | 9.679 | 0.000 | 0.909 | 1.128 |
| 2 | 435 0.0408 | 2.178 | 10.831 | 0.000 | 1 036 | 1 302 |









| Proposed Ideal-CT | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
|----------------------|------------------|--------|---------------|---------|---------|---------|
| Voids | % | 7.0 | 6.5 - 7.5 | 7.1 | 7.0 | 7.0 |
| Thickness | mm | 62.0 | 61.0 - 63.0 | 62.1 | 62.2 | 62.0 |
| Diameter | mm | 150.0 | 148.0 - 152.0 | 150.0 | 150.0 | 150.0 |
| Peak Load | kN | | | 13.2 | 10.2 | 12.6 |
| Displacement (L) | mm | | | 6.2 | 6.5 | 6.3 |
| Tensile Strength | kPa | | | 901.7 | 697.5 | 858.9 |
| Fracture Energy (Gf) | J/m ² | | | 9,825.1 | 8,066.7 | 9,413.7 |
| Slope (S) | kN/mm | | | 2.32 | 1.65 | 2.25 |
| Gf/S | | | | 4,235.4 | 4,999.7 | 4,225.4 |
| (Gf/S)*(L/D) | | | 70 - 250 | 176.0 | 217.5 | 178.8 |







AASHTO TP 124

Standard Method of Test for Determining the Fracture Potential of Asphalt Mixtures Using Semicircular Bend Geometry (SCB) at Intermediate Temperature

| Mix Type: 9.5 F3 6 Test Temperature: 25C | Mix Type: 9.5 F3 64S-22 20% RAP est Temperature: 25C | | | | | Date Tested: 05/30/19 Technician: Greg Rose | | | |
|---|---|--------|--------|--------|---------|--|---------|--|--|
| Specimen ID | L4A1 | L4A7 | L4A8 | L4A10 | Average | Standard Deviation | COV (%) | | |
| Air Voids (%) | 6.6 | 7.2 | 7.4 | 7.1 | 7.1 | 0.3 | 4.8 | | |
| Thickness (mm) | 48.40 | 49.10 | 48.00 | 49.00 | 48.6 | 0.5 | 1.1 | | |
| Ligament Length (mm) | 58.50 | 55.90 | 58.10 | 57.90 | 57.6 | 1.2 | 2.0 | | |
| Max Load (kN) | 4.12 | 3.63 | 3.90 | 3.34 | 3.7 | 0.3 | 9.0 | | |
| Fracture Energy, Gr (J/m ²) | 2413.5 | 2462.4 | 2632.7 | 2799.2 | 2576.9 | 175.4 | 6.8 | | |
| Slope (kN/mm) | -4.74 | -2.53 | -3.67 | -2.41 | -3.34 | 1.09 | 32.8 | | |
| Elevibility Index (El) | 5.09 | 9.73 | 7.17 | 11.60 | 8.4 | 2.9 | 34.0 | | |

8

Minimum Flexibility Index (FI) Criteria





This report was developed using the Rutgers Asphalt Analysis Tool-Pack (RAAT-Pack)







SEMICIRCULAR BEND (SCB)

| Semicircular Bend (SCB) | Units | Target | Range | Lot 4A | Rutgers | Lot 4B |
|-------------------------|-------|--------|-------------|--------|---------|--------|
| Voids | % | 7.0 | 6.0 - 8.0 | 7.1 | 7.1 | 7.0 |
| Thickness | mm | 50.0 | 49.0 - 51.0 | 48.6 | 49.9 | 48.8 |
| Ligament | mm | | | 57.6 | 58.1 | 57.9 |
| Max Load | kN | | | 3.75 | 3.30 | 3.28 |
| Fracture Energy | J/m² | | | 2604.3 | 3200.8 | 2513.2 |
| Slope | kN/mm | | | -3.28 | -1.72 | -2.31 |
| Flexibility Index | FI | > 8.0 | | 8.6 | 18.8 | 11.4 |















SPECIAL NOTE ITERATIONS

| | | v 2.00 (2020) | | v 3.00 (2021) | | v 4.00 (2022) | |
|-----------------------------------|----------------------|----------------------|-------------|----------------------|-------------|----------------------|-------------|
| Test Method | Criteria | Min. Design Value | Max. COV | Min. Design Value | Max. COV | Min. Design Value | Max. COV |
| Flexibility Index | Flexibility Index | 6 | ≤ 20 | 6 | ≤ 40 | 8 | ≤ 40 |
| Indirect Tensile Strength Test | IDT Strength | 100 psi | ≤ 20 | 30 psi | ≤ 40 | 30 psi | ≤ 40 |
| Determination of CT Index | CT Index | - | - | 100 | ≤ 40 | 135 | ≤ 40 |







D264122

<u>SPECIAL NOTE</u> D264122 – P.I.N. 9358.39

HMA MIXTURE EVALUATION USING PERFORMANCE TESTING

Description:

This note covers the requirements for asphalt mixture verification and production under a performance testing process. Plant Quality Adjustment Factors do not apply for mixture produced under this note. Department mixture Quality Assurance will consist of paver sampling and review of Contractor control charts.

All provisions of Sections 401 Asphalt Production and 402 Hot Mix Asphalt (HMA) Pavements of the NYS Standard Specifications apply except as modified below.

Mixture Design Process

HMA mixtures shall be designed to meet the requirements of New York State Materials Method 5.16. Additionally, the mixture shall be tested to meet the performance testing requirements specified in *Table 1 - Performance Testing*.

Table 1 - Performance Testing

| Test Methods | Criteria | Design Criteria | COV |
|--|-------------------|-----------------|-----|
| AASHTO TP 124-18 Flexibility Index Test | Flexibility Index | 6 | ≤20 |
| ASTM D6931-17 Indirect Tensile Strength Test | IDT Strength | 100 psi | ≤20 |
| ASTM D8225-19 Determination of CT Index | CT Index | - | - |

Quality Control Process

95A1

The Quality Assurance Technician (QAT) is not required at the HMA Plant. The QAT shall not be responsible for any activities at the Producer Lab.

The test properties described in *Table 2* shall be recorded by the Contractor on control chart templates, provided by the Department. These control charts should be used by the Contractor to identify any changes in the mixture production. These Control Charts will be filled out and submitted to the Regional Materials Engineer daily.

Table 2: Testing and Sampling Table

| Plant Test Property | Test Method | Contractor Testing Frequency *All Sampling at Plant | Department Testing Frequency *All Sampling at Paver |
|------------------------------|-------------------------|--|--|
| Aggregate Gradation | AASHTO T27 | One per Sublot | One per Day (Enough material for two tests will be collected) |
| Aggregate Moisture | AASHTO T 255 | One per Lot | Monitor and Verify |
| Mix Temperature | N/A | Two per Sublot | |
| Air Voids | MM 5.16, AASHTO T269 | One per 3 Lots | One per 3 Days |
| Indirect Tensile Strength | ASTM D6931-17 | One per 3 Lots | One per 3 Days |
| Semi-Circular Bending | AASHTO TP 124- 18 | One per 3 Lots | One per 3 Days |
| Determination of CT Index | ASTM D8225-19 | One per 3 Lots | One per 3 Days |







IDEAL RUT TEST

Development of IDEAL-RT : Concept

□ IDEAL-RT: TWO supports and shear





IDEAL Rutting Test









QUESTIONS?

Greg Rose

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